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## Concentration and flux of wind-blown snow

Malcolm Mellor and Gregor Fellers

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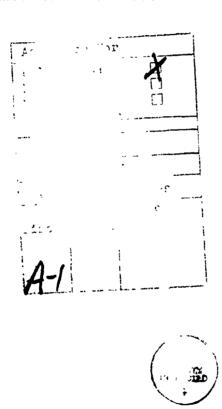
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#### PREFACE

This report was prepared by Dr. Malcolm Mellor, Research Physical Scientist, Experimental Engineering Division, and Gregor Fellers, Computer Specialist, Engineering and Measurement Services Branch, Technical Services Division, U.S. Army Cold Regions Research and Engineering Laboratory. The work was supported as part of DA Project 4A762730AT42, Design, Construction, and Operations Technology for Cold Regions, Task Area BS (Base Support), Work Unit 044, Control of Snowdrifting and Ice Accretion.

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#### CONCENTRATION AND FLUX OF WIND-BLOWN SNOW

#### Malcolm Mellor and Gregor Fellers

Information on the mass concentration and the horizontal mass flux of blowing snow is useful in dealing with certain practical problems, notaby those involving snowdrift formation, wind tunnel (or water flume) modeling of blowing snow, reduction of visibility, and attenuation of radiation near optical frequencies. The basic requirement is for data on the concentration and flux as functions of height and wind speed when the wind blows across a flat surface with an ample supply of loose snow particles.

Many years ago, Australian investigators working in Antarctica gathered a large quantity of systematic data on blowing snow, using techniques and equipment that were validated by tests and theory. Results were analyzed very thoroughly, with emphasis on establishment of the relevant physics. Without doing anything essentially different from the original investigators, we have combined the Australian data and applied multiple regression analysis in order to relate mass flux and mass concentration to the relevant variables that are most easily measured, i.e. height above surface, and wind speed at standard anemometer height.

The Australian studies were inspired by Fritz Loewe, whose interest in blizzards was stimulated by a wintering in Terre Adélie. Systematic observations were originated by M. Mellor and developed under the direction of U. Radok. The great majority of the field observation were made by R. Dingle, and analyzed by U. Radok and W. Budd. Anemometers and aerodynamic snow collectors were mounted in pairs on vertical masts, with logarithmic vertical spacing. At each level, the instruments gave wind speed and mass flux. Mass concentration and the parameters of the wind profile (shear velocity and roughness height) could then be derived. Altogether, 1201 usable data sets were obtained (see Appendix). They include measurements in conditions where: (a) there is new snow falling directly into the turbulent boundary layer, and (b) there is no precipitation from above and all particles are picked up from the surface. Most of the observational

data have been published (Budd et al. 1965, Mellor and Radok 1960), but some unpublished results were provided directly by Dingle and Radok. Information on particle size and fall velocity can be found elecwhere (Budd 1965, Budd et al. 1965, Mellor 1965); with strong winds (> 10 m/s) mean particle size is approximately 100 µm around 1 m height, about 150-200 µm within a few centimetres of the surface, and about 90 µm at head height.

Measurements have been made by other investigators, but we do not have access to the actual observational data, or to the instrument calibrations that are needed to establish comparability.

To obtain representative empirical relations for the dependence of flux q and concentration  $\rho$  on height z and wind speed  $u_{10}$ , we can perform multiple regression analysis on the data while taking account of the relevant physics. The dependent variable Y is a simple function of either q or ρ, and it is expressed initially as a 10-term polynomial with cross-products and terms up to the third power. Some terms may be discarded on the basis of significance tests. The two independent variables  $X_1$  and  $X_2$  are simple functions of z and  $u_{10}$  respectively. If Y is taken directly as  $\rho$ , with  $X_1$  and  $X_2$  as z and  $u_{10}$  respectively, the correlation is very poor, since the observed values of Y range over more than 4 orders of magnitude, while corresponding values of X1 range over more than 2 orders of magnitude. Using the logarithms of the observed quantities for Y and X1, together with u10 as X2, the results are much better. However, both theory and observation (Dingle and Radok 1961, see also Budd et al. 1965 and Mellor 1965) indicate that the relation between ln p and the reciprocal of wind speed,  $1/u_{10}$ , should be close to linear, and it is found that regression of  $\ln \rho$  (Y) against  $\ln z$  (X<sub>1</sub>) and  $1/u_{10}$  (X<sub>2</sub>) gives the best fit to the data:

A parallel treatment for the regression of ln q against ln z and  $1/u_{10}$  is less easy to relate to theory. However, by using different forms of the wind profile in the expressions for  $\rho$  and u in the product  $q = \rho u$ , the logarithmic regression forms for q and z can be justified (see Mellor 1965, p. 15, eq 17). By comparing magnitudes for the two parts of the exponent in the hybrid equation for q, it can be argued that the wind-dependence of q is not radically different from that of  $\rho$ , so that there can be no strong objection to taking  $X_2$  as  $1/u_{10}$  in the regression.

In both regressions the multiple correlation coefficient r = 0.978. The standard error of Y about the regression plane is 0.453 for  $\ln \rho$  and 0.447 for  $\ln q$  (with  $\rho$  and q in units of  $g/m^3$  and  $g/m^2$ -s respectively).

The final regression equations were as follows.

## Mass flux, q

Y = 
$$\ln q$$
,  $X_1 = \ln z$ ,  $X_2 = 1/u_{10}$ . (q  $\ln g/m^2$ -s, z  $\ln m$ ,  $u_{10} \ln m/s$ )  
Y =  $10.089 - 0.41049 X_1 - 122.03 X_2 - 0.13856 X_1^2 - 14.446 X_1X_2$   
 $- 0.0059773 X_1^3 + 3.2682 X_1^2X_2 + 114.13 X_1X_2^2 + 2290.0 X_2^3$ 

## Mass concentration, $\rho$

Y = 
$$\ln \rho$$
,  $X_1 = \ln z$ ,  $X_2 = 1/u_{10}$ . ( $\rho \ln g/m^3$ ,  $z \ln m$ ,  $u_{10} \ln m/s$ )  
Y =  $4.8679 - 0.42209 X_1 - 34.369 X_2 - 0.13265 X_1^2 - 17.427 X_1X_2$   
 $- 972.01 X_2^2 - 0.0070277 X_1^3 + 3.2692 X_1^2 X_2 + 135.54 X_1 X_2^2$   
 $+ 6430.2 X_2^3$ 

Figure 1 shows probable values of mass concentration  $\rho$  as a function of height z and wind speed  $u_{10}$  according to the regression equation. In Figure 1a,  $\rho$  is plotted against z on logarithmic scales, with  $u_{10}$  as parameter. In Figure 1b,  $\rho$  is plotted on a logarithmic scale against  $1/u_{10}$  (or against  $u_{10}$  on a distorted scale), with z as parameter. The observational range for z was from 0.03 to 4 m, and for  $u_{10}$  it was mainly within the range 10 to 25 m/s, with a few values up to 36 m/s.

For high wind speeds, when particles are well diffused, Figure la indicates that the theoretical power relation between  $\rho$  and z is a good approximation, with an exponent not far from -1. The exponent given by simple theory is -w/ku\*, where w is particle fall velocity, u\* is shear velocity (\* 1 m/s with winds of 25-35 m/s), and k is von Karman's constant (0.4). If -w/ku\*  $\approx$  -1 for strong winds, w  $\approx$  0.4 m/s, which is a credible value for particles of wind-blown snow.

At low wind speeds, when there is a sorting of particle size (and fall velocity) with height (see Budd 1965), a linear relation between  $\ln \rho$  and  $\ln z$  applies only at low levels. At the lowest observed wind speeds ( $\approx 10$  m/s),  $\rho$  tends to a limit of about 0.06 g/m<sup>3</sup> when z is greater than a fcw metres. This is the sort of concentration that corresponds to very light snowfall in calm weather. At the lower levels, the general (negative)

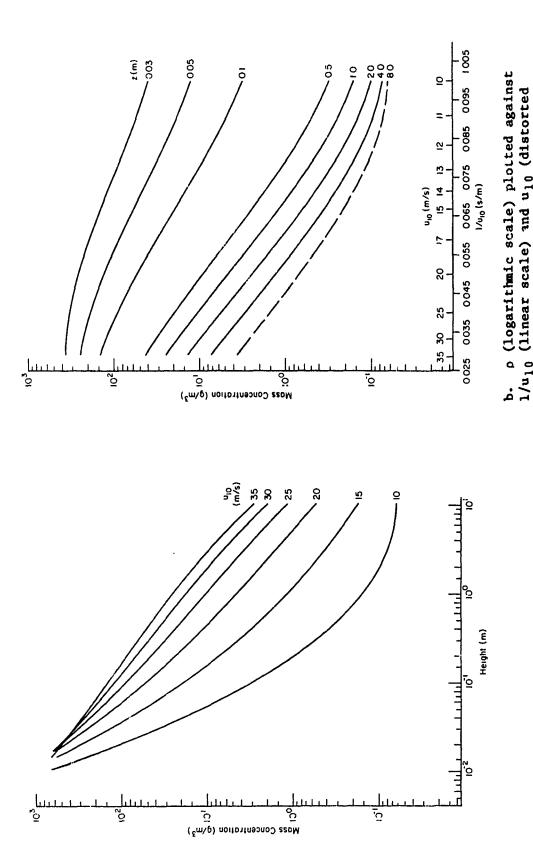


Figure 1. Probable values of mass concentration  $\rho$  as a function of height z and wind speed  $u_{10}$ .

p plotted against z on logarithmic scales,

with ulo as parameter.

The line for

z = 8 m is broken because the highest

measuring level was z = 4 m.

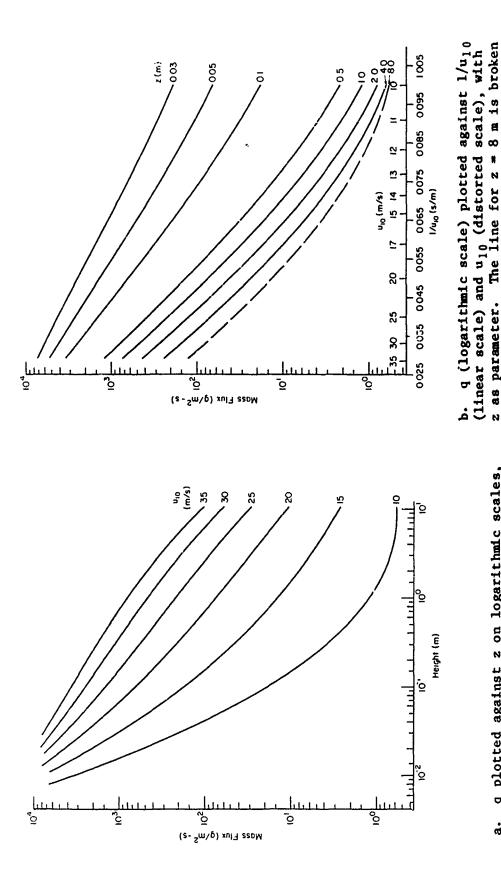
scale), with z as parameter.

slope of the curves in Figure la increases as  $u_{10}$  decreases, presumably because the shear velocity is proportional to  $u_{10}$ . Very close to the ground ( $z \approx 10$  mm), the curves converge to a focus, indicating an upper limit of concentration that is not strongly dependent on wind speed. This limit, which is approximately 1400 g/m<sup>3</sup> and therefore close to air density ( $\approx 1300 \text{ g/m}^3$ ), was predicted and noted in earlier studies (Owen 1964, Budd et al. 1965, Greeley and Iversen 1985). The height of the "focus" is more or less the height of the top of the saltation layer.

Figure 1b shows that the theoretical expectation of inverse proportionality between  $\ln \rho$  and  $1/u_{10}$  is realized in strong winds at levels above 0.5 m. However, with less strong winds the concentration does not decrease as much as might be expected from simple theory, perhaps because falling snow sets a lower limit for  $\rho$ . At low levels,  $\rho$  becomes progressively less sensitive to wind speed, as already mentioned in connection with the "focus" in Figure 1a. The curves for low levels in Figure 1b could perhaps be approximated by straight lines, but they actually show contraflexure. Taken at face value, they suggest that  $\rho$  may become almost independent of  $u_{10}$  for very high winds and for layers very close to the surface, a trend which seems credible. They also indicate a trend towards a lower limit of  $\rho$  in light winds for layers very close to the surface. This is more difficult to rationalize, although one might consider systematic change in particle size as a possible explanation.

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Figure 2 gives horizontal mass flux q as a function of height z and wind speed  $u_{10}$ . The plot of ln q against ln z (Fig. 2a) shows approximate linearity for high wind speeds, with the relation not too far from inverse proportionality. In lighter winds, an approximately linear relation between ln q and ln z prevails only at low levels. At high levels and low wind speeds, q for a given value of z tends towards a limit. As was the case for  $\rho$ , the curves in Figure 2a tend to suggest convergence to a focus very close to the surface, but it is not easy to accept this trend. Extension of the curves to a common point indicates  $q \approx 30,000 \text{ g/m}^2$ -s at  $z \approx 6$  mm. However, the limiting value of  $\rho$  at low level should be approximately  $1300 \text{ g/m}^3$ , with a wind speed of approximately 2 m/s very near the surface. This is an order of magnitude discrepancy; the expected maximum for very low levels is  $q \approx 3,000 \text{ g/m}^2$ -s at z < 10 mm.



Probable values of horizontal mass flux q as a function of height z and wind speed  $\mathbf{u}_{10}$ . Figure 2.

a. q plotted against z on logarithmic scales,

with ulo as parameter.

because the highest measuring level was z = 4 m.

Figure 2b shows approximate inverse proportionality between  $\ln q$  and  $1/u_{10}$  at very low levels, but above 0.1 m there is inverse proportionality only in very strong winds. At the higher levels, there appears to be a trend towards a lower limit of q as  $u_{10}$  decreases. The indication is that such a limit might be of order 0.1 to 1.0 g/m<sup>2</sup>-s, corresponding to the suggested lower limit of  $\rho$  around 0.06 g/m<sup>3</sup> if wind speeds are a few metres per second.

If new measurements should be made in the future, it would be useful to extend the profiles above the 4-m level, since extrapolation to high levels is called for in the treatment of certain problems.

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## APPENDIX A: FIELD DATA USED FOR REGRESSION ANALYSIS

Principal data source: Budd et al. (1965).

Additional unpublished data provided by R. Dingle and U. Radok.

Some data for very strong winds from Mellor and Radok (1960).

Height (z)	Wind er10 m	Mass Conc	Wind e z m	Mass Flux	Height (z)	Wind @ 10 m	Mass Conc	Wind e a m	Mass Flux
4,000	9.60	0.076	8,79	0.668	2,000	12.66	0.564	11.00	6,204
4,000	9.78	0.019	8.95	0.170	2.000	12.68	0.255	11.04	2.815
4.000	10.19	0.111	9.37	1.040	1.000	9.60	0.175	7.5	1.326
4.000	10.73	0.057	9.93	0.566	1.000	9.78	0.173	7.54	0.279
4.000	11.07	0.136	10.28	1.396	1.000	10.19	0.037	8.23	2.066
4.000	11.17	0.735	10.16	2.225	1.000	10.73	0.130	8.59	1.117
4,000	11.21	0.082	10.10	0.839	1.000	11.07	0.150	9.59	2.532
4.000	11.31	0.109	10.23	1.126	1.000	11.17	0.505	8.79	4.439
4.000	11.60	0.104	10.78	1.121	1.000	11.21	0.330	8.90	3.382
4.000	11.64	0.105	10.62	1.115	1.000	11.31	0.385	8.60	3.311
4.000	11.64	0.705	10.75	2.257	1.000	11.60	0.199	9.29	1.549
4.000	11.62	0.046	10.75	0.499	1,000	11.64	0.424	9.24	3.918
4.000	11.87	0.120	10.63	1.300	1.000	11.64	0.691	9.36	6.468
4.000	11.93	0.207	10.85	2.246	1.000	11.62	0.278	9.44	2:624
4.000	11.94	0.103	10.55	1.109	1.000	11.87	0.436	9.56	4.168
4.000	12:08	0.103	10.73	1.105	1.000	11.93	0.362	9.26	3.352
4.000	12.10	0.025	11.18	0.279	1.000	11.94	0.423	9.30	3.934
4.000	12.19	0.150	11.22	1:.683	1.000	11.08	0.218	9.21	2.008
4.000	12.26	0.250	11.27	2.818	1000	12.10	0.205	9.47	1.941
4.000	12.29	0.233	11.26	2.626	1.000	12.19	0.522	9.71	5.069
4.000	12:41	0.050	10.99	0.549	1.000	12.26	0.406	9.69	3.934
4.000	12:41	0.249	1125	2:801	1000	12.29	0.348	9.67	3.365
4.000	12.43	0.140	11.42	1.599	1.000	12.41	0.366	9.34	3.418
4.000	12.52	0.045	11.65	0.524	1.000	12.41	0.759	9.62	7.302
4.000	12.56	0.582	11.53	6.710	1.000	12.43	0.484	9.73	4.709
4.000	12:56	0.161	11.70	1.884	1000	12.52	0.163	10.29	1.677
4.000	12.66	0.264	11.74	3.099	1.000	12.56	0.821	9.74	7.997
4.000	12.68	0.095	11.84	1:.125	1:.000	12.56	0.553	10.14	5.607
2.000	9.60	0.122	8.43	1.026	1.000	12.66	0.906	10.07	9.123
2.000	9.78	0.031	8.28	0.257	1.000	12.68	0.544	10.05	5.467
2.000	10.19	0.176	8.90	1.566	0.500	9.60	0.331	7.11	2.353
2.000	10.73	0.091	9.17	0.834	0.500	9.78	0.120	6.99	0.839
2.000	11.07	0.230	9.79	2.252	0.500	10.19	0.271	7.61	2.062
2.000	1117	0.410	9.75	3.997	0.500	10.73	⊙.354	7.92	2.804
2.000	11.21	0.205	9.61	1.970	0.500	11.07	Ö:541	8.82	4.772
2.000	11.31	0.236	9.57	2.259	0.500	11.17	0.889	8.32	7.396
2.000	11.60	0.149	10.06	1.502	0.500	11.21	0.791	8.06	6.375
2.000	11.64	0.226	10.11	2.285	0.500	11.31	0.422	7.48	3.157
2.000	11.64	. 0.336	10.02	3.367	0.500	11.60	0.363	8.77	3.184
2.000	11.62	0.074	10.20	0.755	0.500	11.64	0.655	8.46	7.233
2.000	-11.87	0.221	10.19	2.252	0.500	11.64	1.133	8.57	9.710
2,000	11.93	0.223	10.20	2.275	0.500	11.82	0.420	8.69	3.650
2.000	11.94	0.223	10.25	2.286	0.500	11.87	0.861	8.65	7.448
2.000	12.08	0.141	9.94	1.402	0.500	11.93	0.790	8.54	6.747
2.000	12.10	0.068	10.32	0.702	0.500	11.94	0.659	8.44	5.562
2.000	12.19	0.296	10.37	3.070	0.500	12.08	0.590	8.09	4.773
2.000	12.26	0.322	10.40	3.349	0.500	12.10	0.478	8.65	4.135
2.000	12.29	0.286	10.41	2.977	0.500	12.19	1.006	8.88	6.933
2.000	12.41	0.110	10.23	1.125	0.500	12.26	0.566	8.99	5.088
2.000	12.41	0.429	10.53	4.517	0.500	12.29	0.464	8.85	4.106
2.000	12.43	0.241	10.86	2.617	0.500	12.41	0.544	8.26	4.493
2.000	12.52	0.068	10.87	0.739	0.500	12.41	1.151	8.77	10.094
2.000	12.56	0.759	10.93	8.296	0.500	12.43	0.734	9.11	6.687
2.000	12.56	0.275	10.75	2.956	0.500	12.52	0.507	9.76	4.948
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, id 1873	;	176.490	57.070	72.670	99.350	51.030	56.170	70.860	102.200	960.0	0.128	0.143	0.348	0.158	0.118	0.473	0.187	0.371	0.358	0.185	9 0.0	0.091	0.437	0.425	0.135	0.392	0.180	0.132	0.224	0.356	0.441	0.310	7 9 0 0	9 9	9 K	9 6	0.217	1	0.240	0.334	0.540	0.374	6.73		007.0		50.0	101	600	0.632	0.00	1 C	200	<b>8</b>
# 10 m		12.41	12.41	:2,43	12.52	8.5	12.56	12.66	12.68	12.70	12.75	12.77	12.84	12.05	12.90	12.8	12.97	13.12	13.21	13.28	13.28	13.39	13.40	13.46	13.58	13.62	13.62	13.66	13.66	13.80	13.0	 	0		<b>8</b> 8	3 6	8	12.70	12.73	12.77	12.0	12.85	12.90	<b>8</b> 5	12.97	13.12	2.5	13.20	3.50	5.5	3. E.		20.5	79.61
Heught (2)		0.031	0.031	0.031	0.031	0.031	0.031	0.031	0.031	7.000	7.000	4.000	000.	4.000	4.000	000.	7.000	7.000	200.	000; #	000. 7	000.4	000.	000.	4.000	7.000	4.000	7.000	4.000	7.000	90.	0 0 ::	8	9	8 8	3 8	9	2.000	2.000	2.000	2.000	2.000 2.000	2.000	2.000	88.	98.0	3 8	8.6	3 8	8.6	88.6	3 6	200.0	7.7 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0
A STATE		47.478	6.0.04	57.636	52.017	59.377	48.277	43.815	33.355	42.414	60.528	83.950	23.179	79.607	171.790	40.422	147.206	92.768	106.491	76.405	130.101	89.937	159.536	119.021	70.5%	153.259	194.688	202.742	74.682	127.997	162.374	<b>3</b>	1.6.231	103.352	75.75		228 483	323.315	470.407	291.879	300.321	665.510	95.252	506.618	291.716	452.146	11.00	505.75	560.653	23.00	\$5.0% \$1.0%	214.70	5/6.219	617.100
E to a		7.68	8.26	7.89	8.2	9.0°	8.17	5.42	5.55	5. <b>8</b> 9	8.9	7.16	6.15	5.9 <b>8</b>	2.67	6.78	6.38	6.57	6.59	6.49	6.18	60.9	5.26	6.50	6.62	9.9	S	5.27	6.27	6.93	7.56	7.96	7.20	2.2	۲. ا	<b>6</b> .	, c	i N	2	5.47	χ. Ά	8	6.12 2	5.67	6.0	e G	: i	٠ ا	n :			, ,	3 8	2.0
dess Conc		2119	4.849	7.305	6.543	7.758	5.909	8,084	6.605	7.201	10.088	11.726		13.290	30.298	5.962	23.073	14.120	16.463	11.705	21.052	14.766	30.330	16.311	10.664	23.221	29.92	38.471	11.911	18.470	21.478	11.635 25	2.73	8	29.			90.320	70.210	53.360	56.030	135.820	30.270	103.460	9.360	7.290	20.5			54.121	047.07	9.5	81.55	36.75
Wind @ 10 m		12.43	12.52	12.56	12.56	12.56	12.68	9.50	9.70	10.19	10.73	11.07	11.17	11.21	11.31	9.1.	11.64	11.64	11.82	11.87	11.93	3	12.00	12.10	12.19	12.26	12.29	12.41	2.	12.43	12.52	12.56	12.56 5	<u>7</u>	ğ.	9 f	) - C		11.07		11.21	Ę.	<b>S</b> :	3.	19.1	28	70.1	5	<b>.</b>	12.08	12.10	12.19	12.26	G-71
Height (2)		5,1,0	0.125	0.125	0.135	0.125	0.125	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.082	0.062	0.062	0.062	0.062	0.062	0.062	0.062	0.062	.0 .0	0.0	0.062	0.062		0.062		8 0 0	5	3 6	0.0	0.031	6	0.031	0.031	0.031	0.031	0.03	0.031	5.03	0.0	5.0	0.031	0.031	0.031	0.031	0.031
Mass Flux		12.639	9.761	15.378	8.472	8.131	1.421	4.673	5.358	9.540	11.682	12.902	7.357	5.348	14.101	17.658	7.469	14.218	19.646	11.321	8.697	10.885	17.918	8.915	9.041	9.080	18.500	15.278	3.695	24.782	15.926	32.611	98.	10.782	o (	)     		10	8.	32.561	15.906	39.297	<u> </u>	21.710	96.490	33.673	20.00	9.50	0/0/6	55.75	22.22	96.15 15.15	155.14	39.673
Wind © 2 a		6 0	9.44	44.6	9.66	6.60	6.43	7.08	7.34	9.14	7.45	7.63	7.27	7.97	7.86	9.10	7.98	7.97	7.75	77.77	7.17	8.19	8.28	8.09	8.18	7.37	76.2	8.54	2	8.65	<b>8</b> .59	<b>8</b>	<b>%</b>	v.	v .	<b>9</b> (	o v	- 40	9.9	4. 9.	7.43	7.11		7.29	7.24	9. 6 9. 1	76.9	0 r	7.4	7.42	7.57	7.27	6.33	7.11
Mass		1.359	1.034	1.629	0.877	1.232	0.221	0.660	0.730	1.172	1.568	1.691	1.012	0.671	1.7	2.180	0.936	1.784	2.535	1.457	1.213	1.329	2.164	1.102	1.203	1.232	2,330	1.789	1.551	2.865	<u>.</u>	3.689	1.896	8	<b>C</b>	3.0	)	10 P	3.861	5.056	2.141	5.527	4.737	2.978	0.0	4.839	7	4.312 Att	i i	7	4.075 C. C. C.	4.973	6.5 <b>6</b> 2	0.00 0.00
Wind @ 10 m		12.56	12.56	12.66	12.68	۰. د	9.78	10.19	10.73	11.07	11.17	11.21	11.31	11.60	11.64	11.64	11.82	11.87	11.93	11.94	12.08	12.10	12.19	12.26	12.29	12.41	12.41	12.43	2.52	12.56	12.56	12.66	12.68	6 6	Ø (	2 6	2 6	11.17	11.21	11.31	1.60	1.6 19.	3	11.82	11.87	1.93	<b>T</b>	9.5	2.5.	7.7.	27.59	12.29	12.41	14.2
Height (2)		0.500	0.500	0.500	0.500	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	250	0.250	0.250	0.250		ν. Σ		) <u>(</u>	, ()	0.10	o.125	ة. الأ	0.125	<u>.</u> K	57.0	0.125	0.12	01.0	S S		0.15 C 1	0 0 1 0	51.0	0.15 0.15	0.12 C

nada Arta	7.6. 116 2.7. 113 2.7. 1	539.963 1180.170 614.866 682.259
e i a	\$\frac{1}{2}\frac{1}\frac{1}{2}\f	6.19 7.05 6.63 6.20
,555 Got	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	87.070 167.400 92.740 108.640
#131d @ 10 %		2.2.2.2.2.2.3.8.38
engradi (2)	00000000000000000000000000000000000000	0.031 0.031 0.031 0.031
Mary Flux	20.043 20.043 20.544 20.545	44.911 79.718 37.611 86.450
E PC N No.	ゝ෫෫෫෫෫෫෮෮෮෮෮෫෫෫෮෮෮෮෧෧෧෫෫෧෧෧෧෧෧෧෧෧෧෫෫෫෫෫෧෧෫෫෫෫෫෫	7.7. 7.66 7.9.66 7.22. 2.22.
<b>Pa</b> ss Conc	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5.628 10.407 4.731 10.517
Wind @ 10 m		8.5.5.5 8.6.5.5.5
- <del> </del>	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	-0-0-0 -0-0-0 -0-0-0 -0-0-0
Mass Flux	3.430 3.430 3.430 3.430 3.431 3.431 3.431 3.431 3.432 3.433	19.820 11.230 6.954 8.442
puin e ? e	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0
Mass	0.328 0.327 0.327 0.327 0.266 0.277	0.751
Fu B	2.5.5.6.5.5.5.5.6.5.4.4.5.5.5.5.5.5.5.5.5	13.23 13.28 13.28 13.28 29.28
He1 705	2. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	

Made 5 F Max	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	90.205
3 4 6 7	7.7.7.2.5.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	9 9 0 1 8 8 8 1 8 8 8
Mass Table	2.559 2.259	8.707 8.707
Para e	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.
Height (2)		
May.". Flux	1. 1. 28. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	20.537 30.083
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ite ight		
Mass	603.300 631.865 1419.310 5076.303 5077.046 649.796 649.796 622.418 622.418 622.418 622.418 622.418 622.418 622.418 623.456 623.418 623	6.09 6.09 7.77 7.88 7.79 8.19 8.19 8.19 8.19 8.19 8.19 8.19 8.1
43.20 6.2.3	ႜၟၟၟၟၜၟၜၟၜၟၟၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟၜၟ	1.0.0-1 5.5-E-6
Sec.	124 .93 105 .493 177 .693 177 .69	0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.
Find Fire	8 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	7.7.7.7. 7.7.8.2.7. 7.7.8.2.5.
Height (2)		ġ-ġ-ġ-a 6-6-6-6 6-6-6-6

Mass Flux	5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5	33.886 55.964 20.068 21.688 37.157
Kind e z a	8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.	16.37 16.46 16.21 16.43 16.70
<b>Mass</b> Conc	0.353 0.554 0.452 0.657 0.957 0.957 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 0.619 1.722 1.408 0.639 0.639 0.639 0.639 0.639 0.639 0.639 1.722 1.408 1.408 1.522 1.408 1.522 1.409 1.522 1.409 1.522 1.409 1.522	2.070 3.400 1.236 1.320 2.225
Wind @ 10 m	7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7	19.11 19.39 19.46 19.66
(Z)	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	7.000 7.000 7.000 7.000 7.000 7.000
Mass Flux	212.256 272.497 272.497 272.497 459.780 4112.780 511.428 351.428 359.623 369.625 588.626 588.6466 588.646 588.	11.398 3.348 18.592 3.927 10.552 11.899
# # # # # # # # # # # # # # # # # # #	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
<b>ກ່ອ</b> ຮຣ ຕັ້ນຄວ	25.728 26.918 60.698	0.720 0.218 1.195 0.250 0.855 0.746
Wind @ 10 m	\$\frac{1}{2}\langle \frac{1}{2}\langle \frac{1}{2}\	16.91 17.04 17.07 17.20
Height (2)	0.052 0.052	0:0:0:0:0
Mass	25, 119 126, 136 126, 136 126, 136 126, 136 126, 136 126, 136 126, 136 126, 136 126, 136 136, 136 137, 138 138, 13	174.180 229.670 260.971 302.027 439.382 390.172
6 7 10 10 10 10 10 10 10 10 10 10 10 10 10	30-1-0-0-0-1-0-0-1-1-0-0-0-0-0-0-0-0-0-0	7.77 7.92 7.93 8.26 8.26 8.69
Mass Conc	7.030 7.235 7.235 7.235 7.235 11.659 10.336 10.336 10.336 10.336 10.336 10.336 10.336 10.336 10.336 11.694 11.694 12.079 11.694 12.079 14.035 15.046 16.906 17.021 18.753 18.753 19.907 22.391 19.907 22.391 10.356 20.956 20.	22.417 29.905 33.415 36.743 53.194 14.899
Purd e	5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.	14.41 14.45 14.55 14.66
Herght (2)	0.000 0.000	0.062 0.062 0.062 0.062 0.062

Mars Flux	3696.524 3073.590	5301.750	5641.952	759.54	5,889	43.625	133.400	067-107	36.326	89.686	80.643	16.73	67.	262	4.539	52.957	16.754	71.401	4.527	71.698	28.000 00.000	92.979	192.02	346.060	13.99	140.013	161.014	200. ECC	183.976	71.315	7.760	101.979	€. 8 . 8	7.58	106.141	15.523	97.945	263.015	519.935	505.100	229, 181	237.057	125.516	293.109	307.692		
E nd	\$ 01.5	10.43	10.36	18.55	13.76	21.49	8.8	8,8	19.22	22.31	22.91	21.97	24.92 84.92	70.01	15.49	22.43	21.73	23.88	17.20	17.31	11.82	\$ 6 8.1	25.50	26.03	18.18	20.98	21.70	21.5	24.4 74.4 74.4	18.62	14.81	21.56	29.1e	16.72	9	12.31	19.55	17.80	22.44	60.47	97.71	7	200	23.83	23.10	İ	
<b>Pass</b> (2)194	371.510	505.410	544.590	348.970	0.428	2.030	6.670	11.250	0.00	4.020	3.520	2.220	064.9		200	7.361	0.77	2.990	0.262	4.142	6.599	1.540	10.160	17.350	3.520	9.680	7.420	3.740	7.730	3.830	0.524	4.730	2.267	201.4		1.261	5.010	14.710	23.170	22.570	6.450	0.1.	- 4	12.30	13,320		
e cind	22.43	22.68	73.94	24.05	14.74	22.94	21.69	26.39	29.23	24.28	24.60	23.27	26.27	0 %	2.3	2 2	23.07	75. E	18.22	20.13	14.74	\$2.5 \$	21.69	% % %	20.62	24.28	24.60	23.27	26.27		16.68	24.04	23.07	25.44	22.62	14.74	22.94	21.69	26.89	29.23	20.91	24.28	2 ° °	26.27	27.75	,	
Height (2)	0.031	0.031 0.031	0.031	0.031	3	000	4.000	4.000	000.4	3.5	90.	8	4.000	000.4	96.	3 8	3 3	900	000	2.000	2.000	2.000	2.000	7.00 7.00 8.00 8.00	8.5	80.5	2.000	8 8 8	2.00	888	80.0	2.000	2.000	2.000	8 8	86		000.1	1.000	.00	.000	00.	3:0	3 5	8 8	<u>}</u>	
Xush Flux	98.696	175.507 240,026	310.676	243.957	186.939	214.412	350.298	319.205	359.290	200.063	340 CAF	457.496	596.836	463.480	410.101	378.200	436.936 546 540	050.049	0.000	12 S	739.911	570.055	610.508	890.312	752.270	981.857	138.315	950.174	037.435	072.808	829.614 6111 828	151.976	1613.374	455.209	634.781	252.640	835	645,345	2384.691	1768.355	2895.192	3648.987	3764.135	1043.083	2200.920	3272.312	
E 7	15.07																																										_			CC:20	
Conc	6.973	11.577	19.601	16.199	11.627	11.943	21.115	19.057	21.644	15.010	29.170	3 5 8 5 8 6	2.5 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	% 90.98	28.860	24.400	30.030	41.350	36. 50. 50. 50. 50. 50. 50. 50. 50. 50. 50	7		966.44	62.550	69.070	63.590	90.020	2 8	22.20	76.170	80.300	89.110	00.001 00.001	141.400	126.430	160.430	168.410	131.300	057.601 0EH 3E1	196.890	151,530	310.310	365.630	365.450	106.340	299.290	382.750	
Wind Flom	20.17	8.8	22.00	22.20	22.43	21 E	22.60 12.60	23.94	24.02	20.17	8.8	<b>8</b> 8	22.5	22.20	22.43	22.62	22.86	23.51	<b>3</b>	7.0	? % ? %	8	22.08	22.13	22.20	22.43	22.62	0. EC	23.94	24.02	20.17	8 8 8 8	22.00	22.13	2 2 2 3	25. 1.53	22.62	22.00	10.02	20. 10.	20.17	20.98	8 8	22.08	22.13	22.20	
Heignt (2)	009:0	0.500	0.00	900.0	ە ق	000	000	000	0.500	0.250	0.25 20.00			200	0.250	0.250	0.250	0.250	0.250	9:10	0.0	2 2 1 1 1		0.125	0.125	0.125	Ç.		0.125	0.125	0.062	0.062	0.062	0.062	80	0.0	0.062	0.00	0.00	3 6	0.031	0.031	0.031	0.031	0.031	0.031	
S. L. L.	1796.456	1493.305	1514.326	1782.166	1360.239	1983.663	2161.910	2012.544	714.7007	1557.785	2086.384	2061.421	2782.233	4093.067	17.864	35.754	30.378	39.117	47.167	₹ .00. 1	29.055	40.571	37.5	62.570	60.703	77.227	.2.668	20 00 00 00 00 00 00 00 00 00 00 00 00 0	50.03 60.03	75.020	146.881	62.884	67.973	7.7	05.50	51.654	123.215	101.399	125.227							202.060	
2 d	8.31	7.35 6.42	7.63	7.62	9 5 5 5	, t	8.16	7.68	, c	96.6	₹ 6	8	ξ. (2)	9.00	9. 4	19.12	19.30	20.06	20.20	19.85	20.29	20.87	20.78	21.57	21.82	17.32	<u>5</u>	8 8	3 1	18.62	18.73	19.59	19.36	3.0	? ? ?	15.04	16.53	16.62	17.48	17.27	16.79	0 - 0 - 0	2	2 6	18.28	18.57	
#1-10 10 4 12 1 12 1	216.180	190.230 277.290	198.470	233.880	148 660	235.310	264.940	262.050	300.630	123.860	233.600	227.530	338.060	475.160	355.920	1 820	1.574	9	2,335	2.242	1.432	1.944	1.783	2.826	2 782	1.572	4.017	3.279	3.2 <u>4</u>	200	2.503	3.210	3.511	6.185 5.05	6 c	3.261	7.454	6.101	7.164	2.947	7.507	u - 6	8 0	200-1	10.367	10.881	
in the second se	17.76	17.79	17.98	6.05 6.05		18.39	.8.42.	*8.42	.8.57	18.65 Co.87	19.6	9.39	97.6	99.61	19:81	20.00	5 5 5 8	20.00	22.13	22.20	22.43	22.62	22.88	23.51	, c	20.17	20.95	20.96	22.08	22.13	22.43	22.62	22.88	23.51	3 S	20.17	20.95	20.96	22.08	22.13	22.20	22.43	7.50	22.00 22.00	10.00	24.02	
Trans.	5.031	0.031	.031	0.031	55	50.0	0.031	0.031	5.031	150.0	0.031	0.031	0.031	0.031	0.031	3 8	3 8	3 8	3 8	88	0	8.	7.000	000	3 5	30	8	2.00	80.0	8 8	36	8.8	2.000	8	88	3 8	8	80.	000.1	8.	8.8	8	8	88	3 8	88	

Mass	2.73.600 3.47.600 53.700 53.700 11.4.610 179.025 578.790 1915.220 1456.320
e u	ន្ត
	15.200 13.500 13.500 17.000 17.050 17.050 17.050 136.600 18.800
E O	%&%&& <b>%</b> & <b>%%</b> 8888888888888
Height (2)	
Mass	1069.958 588.057 111733.511 849.949 1017.967 333.021 111.956 331.956 147.031 311.956 2599.000 3399.000 2599.000
e grad	27 - 77 - 73 - 74 - 74 - 74 - 74 - 74 - 7
Mass Conc	82.750 48.700 54.700 54.700 52.700
Wind @ 10 m	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.
Height (z)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Mass	104.052 18.486 147.351 48.013 173.617 22.80 142.996 159.997 142.996 159.997 140.017 159.997 159.997 159.997 159.997 159.997 159.997 159.997 159.997 159.997 159.997 159.993 159.998 159.998 159.998 159.998 160.312 160.312 176.312
Wind @ z m	2000 200 200 200 200 200 200 200 200 20
Mass Conc	5.980 1.300 1.300 11.660 11.660 11.660 11.660 11.660 10.577 10.310 10.31
Wind e 10 m	28888888888888888888888888888888888888
feright (E)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0